

ARMY RESEARCH LABORATORY



Dispersion Analysis of the XM881 Armor-Piercing, Fin-Stabilized, Discarding Sabot (APFSDS) Projectile

by Thomas F. Erline
and Man F. Hathaway

ARL-MR-433

January 1999

19990330 104

Approved for public release,; distribution is unlimited.

DTIC QUALITY INSPECTED 4

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

Citation of manufacturer's or trade names does not constitute an official endorsement or approval of the use thereof.

Destroy **this** report when it is no longer needed. Do not return it to the originator.

Army Research Laboratory

Aberdeen Proving Ground, MD 21005-5066

ARL-MR-433

January 1999

Dispersion Analysis of the XM881 Armor-Piercing, Fin-Stabilized, Discarding Sabot (APFSDS) Projectile

Thomas F. Erline

Weapons and Materials Research Directorate, ARL

Alan F. Hathaway

Arrow Tech Associates

Abstract

This study compares the results of a dispersion test with mathematical modeling. A 10-round group of modified 25-mm XM881 armor-piercing, fin-stabilized, discarding sabot (APFSDS) projectiles was fired from the M242 chain gun into a designated target. The mathematical modeling results come from BALANS, a product of Arrow Tech Associates. BALANS is a finite-element lumped parameter code that has the capability to model a flexible projectile being fired from a flexible gun. It also has the unique feature of an automated statistical evaluation of dispersion. This study represents an effort to establish a combined experiment and simulation approach to reduce system error.

Acknowledgments

Mr. **T. Marrs** of the U.S. Army Aberdeen Test Center (ATC) **performed** centerline measurements. Mr. **B. Hudler**, **from** the U.S. Army Research Laboratory (ARL), performed projectile measurements. Mr. **B. Patton** (ARL) performed testing with Mr. **D. McClelland** of Defense Services, Inc. Mr. **B. Guidos** (ARL) performed the jump analysis and provided the authors with constructive guidance. Mr. **K. Soencksen** (ARL), Dr. **P. Plostins** (ARL), and Mr. **R. Whyte** of Arrow Tech contributed to the yaw analysis.

INTENTIONALLY LEFT BLANK.

Table of Contents

	<u>Page</u>
Acknowledgments	iii
List of Figures	vii
List of Tables	vii
1. Introduction	1
2. Experimental Approach	2
2.1 Overview of the Experiment	2
2.2 Description of the XM881	2
2.3 Bore Straightness	4
2.4 Experimental Results	4
3. Analytical Approach	6
3.1 Overview of BALANS	6
3.2 BALANS Model of the XM881	8
3.3 Deterministic Analysis	10
3.4 Stochastic Analysis	11
4. Comparison Between Experimental and Analytical Results	14
5. Summary and Conclusions	15
References	17
Distribution List	19
Report Documentation Page	23

INTENTIONALLY LEFT BLANK.

List of Figures

<u>Figure</u>	<u>Page</u>
1. Jump Test Instrumentation	3
2. XM881 Flight Vehicle at Mach 4.0	3
3. M242 Barrel SN 273 for the 25-mm Chain Gun	4
4. The 25-mm XM881 Means of Jump Components	5
5. The 25-mm XM881 Dispersion of Jump Components	5
6. Analytical Approach to Predicting Dispersion	7
7. Graphical Representation of the XM88 1 Lumped Parameter Model	9
8. Interaction Forces: (a) Straight Centerline, (b) SN 273	11

List of Tables

<u>Table</u>	<u>Page</u>
1. XM88 1 Sensitivity Data	12
2. Manufacturing Tolerance Information	13
3. Simulated TID Results of 10 Simulations of 10-Round Tests	13
4. Components of Dispersion (From Simulation No. 3)	14
5. Total Dispersion Comparison.....	15

INTENTIONALLY LEFT BLANK.

1. Introduction

The U.S. Army has a need to improve its understanding of the effectiveness of medium-caliber cannon systems. One of the methods for advancement toward this understanding is to perform experimental aerodynamic jump tests and mathematical modeling that simulates the jump tests. One fielded system of major interest is the **25-mm** M242 Autocannon, which is found on the Bradley Fighting Vehicle. This gun system was selected for study by the U.S. and German Defense Exchange Agreement No. 1132. This system is ideal for setup in a small-caliber range, such as the Aerodynamics Range Facility at the U.S. Army Research Laboratory (ARL) at Aberdeen Proving Ground (APG), MD.

The current service round, used with the **25-mm** M242 Autocannon, is the M919 armor-piercing, fin-stabilized, discarding sabot (APFSDS) projectile used for armor penetration. This round has a depleted uranium penetrator that would contaminate the experimental facility. Therefore, the XM881, which has a tungsten penetrator and was a precursor of the **M919**, presents itself as a suitable substitute. The XM881 has a flight vehicle that is geometrically similar to the M919, including matching threads for fitting the sabot; however, the discarding sabot of the XM881 was totally different from the M919. To better emulate the M919, it was decided to replace XM881 sabots with the sabots used on the M919.

The dynamic state of a projectile at shot exit is determined in part by the in-bore launch disturbances experienced by the projectile as it traverses the length of the barrel. A contributing factor is the initial misalignment of the projectile's principal axis and center-of-gravity (CG) offset with respect to the bore centerline. As the projectile is driven axially **downbore** by the propellant gas pressure, it is also forced to travel a lateral path that is determined by static and dynamic curvatures. Tube droop in the vertical plane is a gravity-induced static curve, and the bore straightness profile is a static curve due to the manufacturing processes' inability to produce a perfectly straight bore. The firing of the gun produces an array of complex interdependent events. Axial **travel** of the projectile and propellant gas pressure will impart forces on the gun for recoil and slight bending in the barrel. The projectile reacts in flexure to the massive barrel,

and the barrel responds to the projectile loads. The dynamic lateral path then becomes a boundary condition of projectile balloting.

The balloting analysis program, BALANS, from Arrow Tech Associates, Inc., was chosen for this study because of its multifunctional abilities. It has the capability to perform a single shot deterministic case in either two or three dimensions and target impact dispersion analysis using a stochastic approach.

Under this mission for investigating the experimental performance of the **XM881**, it is believed that good agreement between the experimental results and modeling results with the BALANS program will allow modeling to point to areas that need improvement. This is especially true in the area of gun tube straightness and interactions between the projectile and the gun tube. In this study, for example, both experiment and modeling show the in-bore balloting reactions to be a significant contribution to dispersion.

2. Experimental Approach

2.1 Overview of **the Experiment**. The M242 chain gun was setup at the Aerodynamics Range of **ARL, APG**. A schematic of the test setup is shown in Figure 1. Two eddy probe stations that measure lateral displacements were positioned about the muzzle brake of the gun to capture the muzzle motion. A pressure probe trigger was located just outside of the muzzle to start the experimental equipment. A sabot catcher plate was positioned several meters from the muzzle. Six orthogonal x-ray stations were positioned within 2 ms of the muzzle to capture velocity, yaw, and yaw rates. There were 25 orthogonal shadowgraph stations to measure the flight vehicle motion (see Figure 2). At 100 m from the muzzle, a target setup recorded shot fall. The muzzle displacements, pointing angles, transverse velocity, and angular velocity were determined using data reduction analysis techniques found in **Haug** and Bornstein [1].

2.2 **Description of the XM881**. The **XM881** is a 25-mm APFSDS experimental round that has gone through a number of design iterations. The **XM881** specimens available did not match

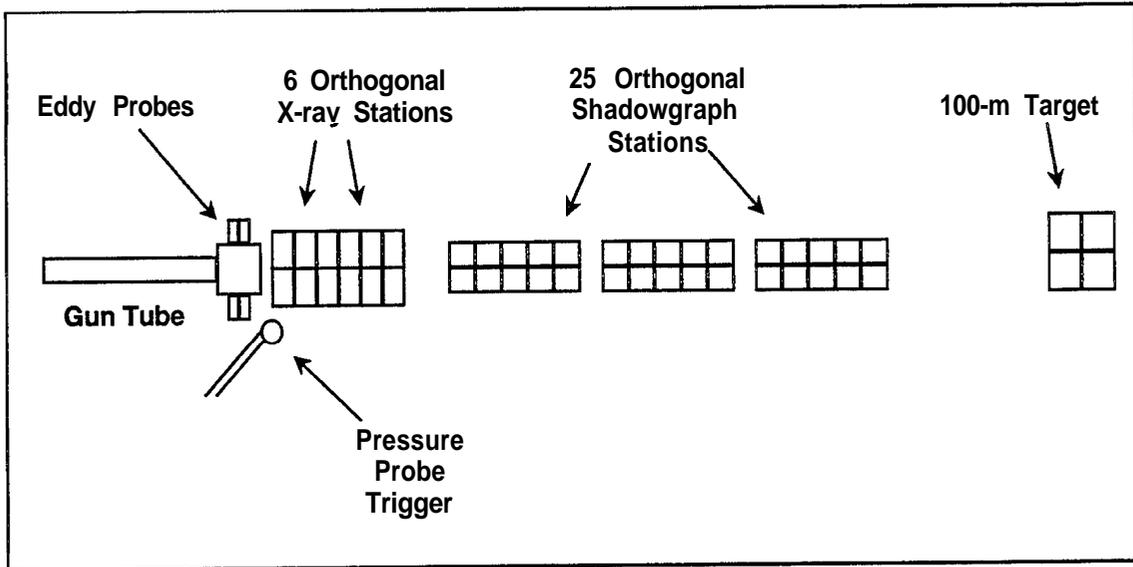


Figure 1. Jump Test Instrumentation.

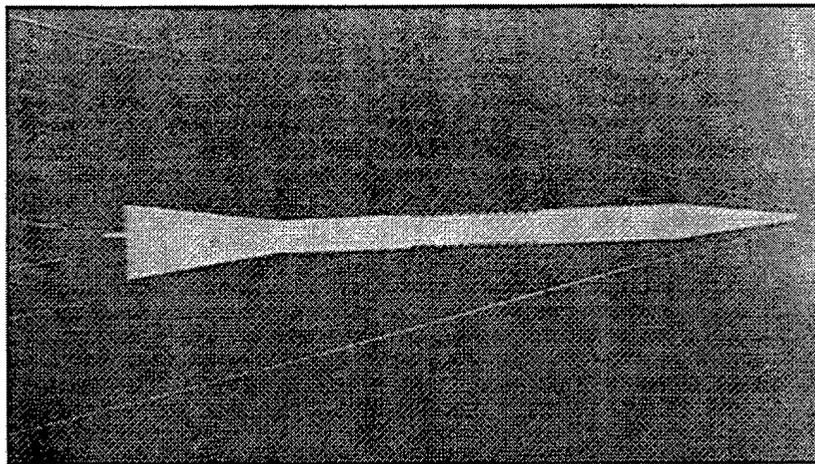


Figure 2. XM881 Flight Vehicle at Mach 4.0.

the particular version of the penetrator drawings found. Therefore, detailed measurements were performed. The total length of the flight vehicle is 153.0 mm with the penetrator length of 82.8 mm and threaded length of 29.4 mm starting at 64.4 mm from the base of the flight vehicle. (Refer to Figure 2 showing a print of a shadowgraph of the flight vehicle from the test.) The original sabots were removed from the flight vehicle and replaced with those found on the M919.

2.3 Bore Straightness. The M242 chain gun was set up with barrel serial number (SN) 273, which was measured for centerline straightness and bore gauged for service condition. The vertical (without gravity droop) and horizontal centerline referencing the rear face of the tube (RFT) of SN 273 is shown in Figure 3. The manufacturing irregularities noted in the centerline are typical with positive up and to the gunner's right.

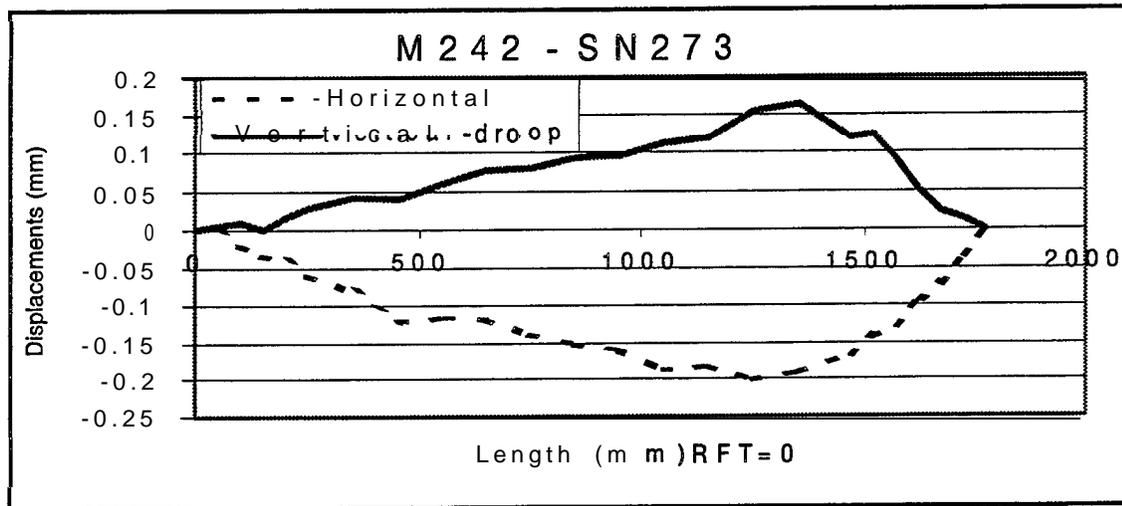


Figure 3. M242 Barrel SN 273 for the 25-mm Chain Gun.

2.4 Experimental Results. The experimental results are utilized in jump and dispersion models that are defined in Plostins et al. [2]. The means of major angular components of jump and dispersion are displayed in Figure 4 in milliradians. The muzzle pointing angle component is noted as “PA.” The muzzle of the gun has transverse velocity noted as “CV,” which imposes on the projectile at shot exit. The angular deviation of the projectile center of gravity relative to a coordinate system attached to the muzzle at shot exit is known as projectile “CG” jump. The “CG” jump is caused by in-bore balloting, muzzle blast, projectile mechanical disengagement, and sabot discard. The component noted as “AJ” is aerodynamic jump, which is the mean angular deviation of the projectile swerve trajectory. There was no measurable evidence of disturbance from sabot discard on the projectile “CG” jump. The sabot discard was completed within 0.15 m from muzzle, which is too close to the muzzle to capture in the x-ray stations. In Figure 4, positive is up and to the right.

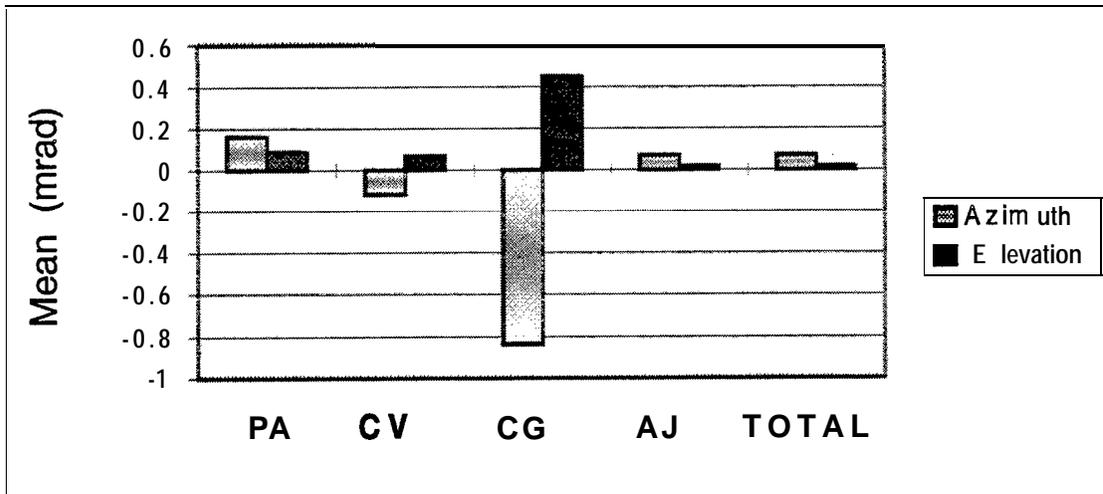


Figure 4. The 25-mm XM881 Means of Jump Components.

The standard deviations of the components of jump are displayed in Figure 5. The dispersion model may be simple if the total dispersion is the result of the sum of the independent individual jumps. The square of the standard deviations of the individual jump components will sum to the square of the impact dispersion. This empirical model appears to be best suited for this type of experiment.

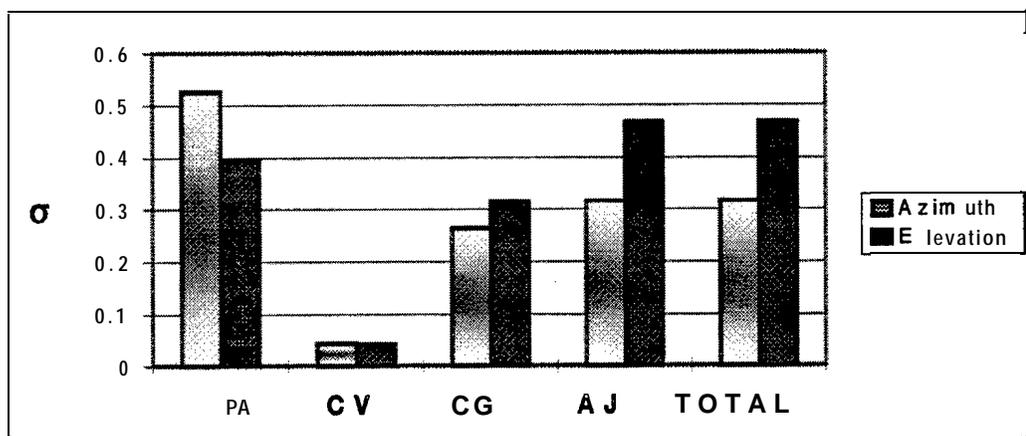


Figure 5. The 25-mm XM881 Dispersion of Jump Components.

3. Analytical Approach

3.1 Overview of BALANS. BALANS [3] simulates the dynamic response and interaction of a flexible projectile and a flexible gun tube during in-bore travel. It also includes the effects of a curved bore profile. The simulation utilizes individual models of the projectile and gun tube, in a time step iterative solution. Pertinent motion and load data are periodically saved during the analysis to produce selective summary graphical displays. BALANS takes advantage of the interior ballistics simulation and CG offset calculations of **PRODAS** [4] and an automatic lumped parameter modeling capability to assist in building a BALANS model.

The analytical procedure utilized in BALANS presupposes that the projectile is initially misaligned within the gun tube due to manufacturing tolerances. During firing, this misalignment produces secondary forces, causing transverse displacement and yawing motion of the projectile as it travels from breech to muzzle. The resulting yaw angle, angular rate, and transverse velocity at muzzle exit are then analyzed for their effects on 'dispersion. It should be noted that BALANS calculates the projectile state (yaw, yaw rate, and transverse velocity) at muzzle exit while the experimental setup determines the state of the tube and bore at the projectile exit.

Figure 6 contains a flow diagram of this stochastic method for predicting dispersion. Whether trying to predict dispersion on a new design or solve a dispersion-related problem on a current design the approach is very similar. It begins with gathering basic technical information such as manufacturing dimensional data, assembly drawings and/or specifications, and analytical results from other analyses or tests such as **finite** element analyses or experimental results of the sabot front borerider. This information is critical to building the accurate analytical model of the projectile to be used during all analyses within this approach. From this information, a tolerance study can also be performed for input into the in-bore balloting analysis.

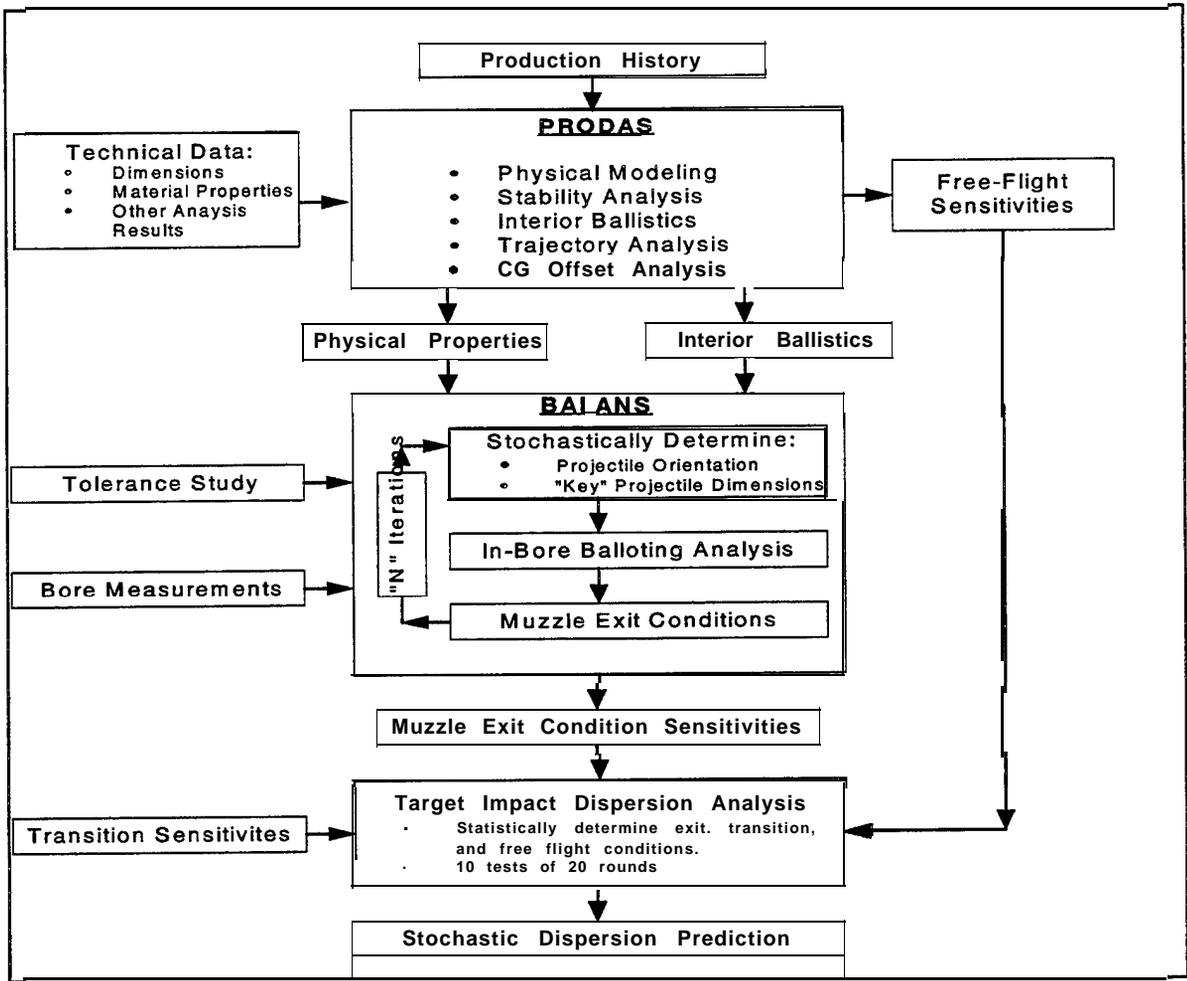


Figure 6. Analytical Approach to Predicting Dispersion.

The second piece of information required is production history information such as Statistical Process Control (SPC) information. Even if working with a new projectile design for which there is no production history, it is valuable to obtain this information for a similar design or a projectile with similar characteristics.

Because some of the inputs to this approach are statistical in nature, the historical data provide a foundation from which to derive the statistical information.

The last type of information required is test and/or measurement that is important to predicting dispersion but is not derived from analysis. This includes bore centerline

measurements, boresight errors inherent within a test fixture or boresight tool, known sabot discard issues from tests of similar sabots, etc.

As can be seen in Figure 6, the drawings, production history, and results from previous analyses are used for physical modeling of the projectile, which in turn is the basis for several analyses to be described in the following sections. Each of the analyses results in dispersion component sensitivities that are then used in predicting dispersion.

3.2 BALANS Model of the XM881. The basic inputs for the BALANS in-bore balloting analysis are a lumped parameter model of the projectile that properly characterizes its mass properties and flexibility, a forcing function, and several distances and runouts that are used to orient the projectile within the gun tube. The lumped parameter model is generated automatically from the PRODAS geometric model.

Figure 7 is an example of the XM881 as a lumped parameter model automatically generated from PRODAS. As shown, the upper half of the model is the actual projectile as generated from PRODAS. The lower half attempts to mirror the upper half by reflecting the lumped parameter node/element model.

The forcing function required for the balloting analysis is provided directly from the PRODAS interior ballistics analysis module. PRODAS uses the Baer-Frankl methodology to simulate combustion of propellant grains and calculate the time-dependent parameters of base pressure (which is applied to the projectile aft of the obturator during the balloting analysis), spin velocity and acceleration (which is used to calculate centrifugal forces during in-bore travel), and axial acceleration (which is used to calculate axial forces during in-bore travel). Transverse forces are calculated from the induced balloting motion.

In addition to the lumped parameter model, the dispersion analysis requires manufacturing dimensional and tolerance information and transition and free-flight sensitivity information. The

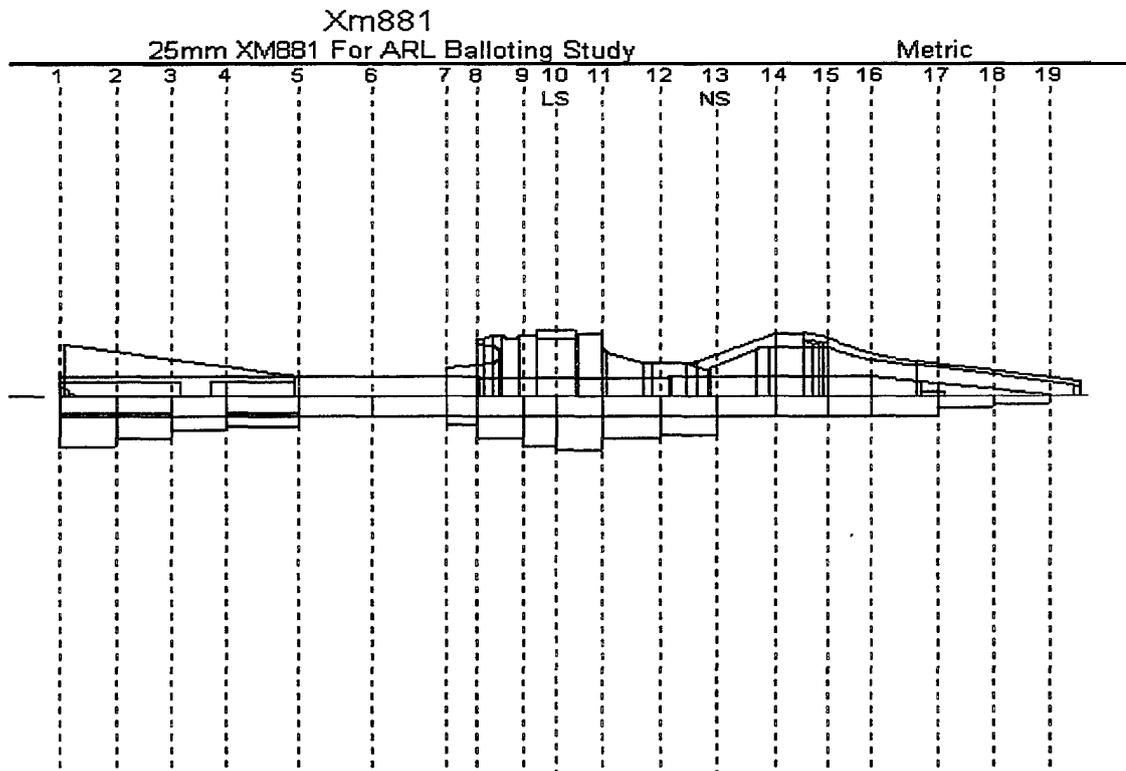


Figure 7. Graphical Representation of the XM881 Lumped Parameter Model.

manufacturing information consists of several critical dimensions and tolerances necessary for in-bore balloting. These define the locations of the projectile/gun tube interfaces and some of the critical projectile dimensions which affect dispersion. The statistical in-bore balloting analysis uses these dimensions and their tolerances to randomly orient the projectile in the gun tube. Several hundred in-bore balloting analyses are generally required to obtain statistically valid muzzle exit yaw, yaw rate, and transverse velocity predictions [5].

The transition and free-flight sensitivity information is used to determine those components of dispersion after the projectile has left the gun tube. Transition sensitivities are separated into sabot discard and boresight sensitivities. Errors induced by sabot discard may have significant variation from one projectile configuration to another. They have both a physical component that can occur due to asymmetric loads applied to the core during discard and an aerodynamic interference component. Sabot discard is the least well understood of the major contributors to dispersion and therefore is generally determined from test, observation, and/or experience.

Boresight errors are the errors associated with pointing the gun at the target. Boresight errors vary between calibers, gun crews, and instrumentation

The free-flight dispersion component sensitivities include muzzle velocity, aerodynamic jump, aerodynamic trim angle, crosswinds, and aerodynamic/mass asymmetries. All of these parameters are determined via trajectory analysis within **PRODAS** as follows:

- The muzzle velocity sensitivity factor is the drop variation due to muzzle velocity variation and can be calculated by comparing the drop of trajectory simulations made by perturbing muzzle velocities.
- The aerodynamic jump sensitivity relates dispersion to the muzzle exit yaw rate of the projectile. This factor is dependent upon the physical and aerodynamic characteristics of the projectile as well as the projectile spin and velocity.
- The crosswind sensitivity of the projectile is determined by trajectory simulations of the projectile flight to the range of interest both with and without a nominal crosswind applied.
- The aerodynamic trim angle of a projectile configuration (due to manufacturing tolerances) may be calculated from **PRODAS** predictions of the body (alone) and fm (alone) center of pressure and normal force coefficients, and from the expected one-sigma **value** of the angular misalignments of the nose and tail sections.
- The aerodynamic/mass asymmetries factor is determined by simulating trajectories with a trim angle assumed to be oriented at orthogonal and diametrically opposed orientations.

3.3 Deterministic Analysis. **Once the** lumped parameter model of the projectile and gun system is finished, one needs to run test cases, starting with the most basic analysis before proceeding to more complex simulations. First, run the simplest case-for example, a two-dimensional single-shot simulation using a straight centerline including gravity droop.

When the results appear reasonable, then move on to a simulation that includes the measured centerline from SN 273. Now, one simple way of obtaining insight from the modeling results is to compare the results from the straight centerline to the measured centerline of SN 273. In Figure 8(a), the projectile lateral forces resulting from interaction with a smooth, straight centerline are shown. Though the loads are low, it is immediately apparent that balloting causes high-frequency disturbance. In Figure 8(b), the projectile lateral forces resulting from interaction with a centerline that includes manufacturing irregularities are shown. The loads are only slightly higher except for some higher forces noted near shot exit delivered to the rear contact of the projectile.

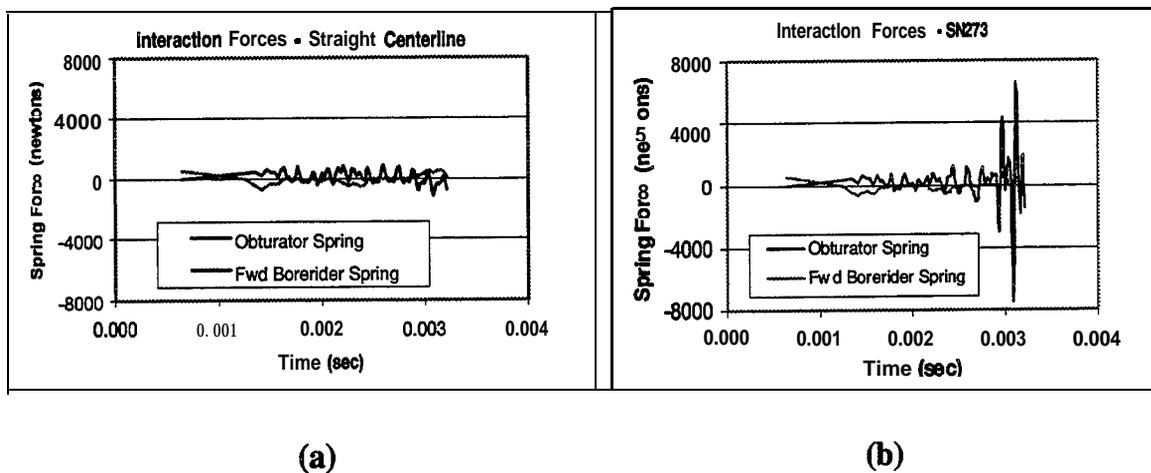


Figure 8. Interaction Forces: (a) Straight Centerline, (b) SN 273.

The deterministic analysis provides a detailed analysis at each node in the lumped parameter model in terms of bending moments, shear forces, nodal displacements, projectile shape at each time step, and exit conditions. It is equivalent to performing a single-shot experiment to investigate issues other than dispersion. Since the analysis presupposes an initial projectile orientation in the gun tube, which is difficult to determine experimentally, the deterministic analysis has limited usefulness when trying to evaluate overall projectile performance parameters such as dispersion.

3.4 Stochastic Analysis. Since production history information such as SPC information does not exist for the XM881 specimens in our inventory, the parameters required for input had to come from either measurements or estimates based on M919 data. For the sensitivity values found in Table 2, the muzzle velocity data come from the experiment. Aerodynamic jump, yaw factor, and spin rate come from the **PRODAS** segment, Boresight, sabot discard, and miscellaneous error numbers are engineering best guess values based on experience with similar projectiles. For simplicity, values that were assumed to be zero, such as wind factors, aerodynamic, and mass asymmetries, are not shown in the table.

Tables 1 and 2 contain sensitivity data and manufacturing information required for the simulation. Generally, these data are obtained from previous simulations, testing, drawings, and/or SPC data collected by the manufacturer. For this simulation, the source of the data was either through measurements (**meas.**) or from engineering estimates (**est.**) that are based on previous experience in simulating and testing of similar rounds.

Table 1. XM881 Sensitivity Data

Characteristic	Value	Data Source
Aerodynamic Jump Factor (dimensionless)	0.030	est.
Muzzle Velocity Standard Deviation (m/s)	8.419	est.
Muzzle Velocity Factor (dimensionless)	0.005	est.
Boresight Error (dimensionless)	0.050	est.
Sabot Discard Error (dimensionless)	0.050	est.
Miscellaneous Errors (dimensionless)	0.100	est.
Muzzle Velocity (m/s)	1398.4	meas.
Initial Yaw Factor (mils)	0.010	est.
Muzzle Spin Rate (rad/s)	2900.0	est.

The **BALANS** dispersion results presented here in Table 3 are the result of 10 different simulations of 10 rounds each stochastically determining projectile orientations and other key

Table 2. Manufacturing Tolerance Information

Characteristic	Value (mm)	Data Source
Distance to Obturator	63.0941	meas.
Distance to Forward Spring	101.143	meas.
Distance to Bore Rider	110.236	meas.
Bore Diameter	25.100	meas.
Forward Bourrelet Mean Diameter	24.970	est.
Forward Bourrelet Standard Deviation	0.015	est.
Forward Bourrelet Runout (Mean to Penetrator)	0.025	est.
Forward Bourrelet Runout Standard Deviation	0.010	est.
Rear Bourrelet Runout (Mean to Penetrator)	0.025	est.
Rear Bourrelet Runout Standard Deviation	0.010	est.
Sabot Inside Diameter at Forward Bourrelet	8.273	meas.
Sabot Inside Diameter at Forward Bourrelet Standard Deviation	0.000	est.
Core Outside Diameter at Forward Bourrelet	8.273	meas.
Core Outside Diameter at Forward Bourrelet Standard Deviation	0.000	est.

Table 3. Simulated TID Results of 10 Simulations of 10-Round Tests

Simulation No.	Horizontal (mrad)	Vertical (mrad)
1	0.320	0.418
2	0.384	0.469
3	0.377	0.463
4	0.350	0.441
5	0.402	0.484
6	0.321	0.419
7	0.460	0.533
8	0.292	0.397
9	0.381	0.467
10	0.408	0.489
<i>Average</i>	<i>0.369</i>	<i>0.458</i>
<i>Standard Deviation</i>	<i>0.050</i>	<i>0.040</i>

dimensions as described earlier to develop the muzzle exit conditions of yaw, yaw rate, and center of gravity velocities. To perform the target impact dispersion analysis, the muzzle exit sensitivities are combined with the transition sensitivities and free-flight sensitivities. Table 4 shows the components of dispersion for one of the simulations.

Table 4. Components of Dispersion (From Simulation No. 3)

Dispersion Component	Horizontal (mrad)	Vertical (mrad)
Yaw Rate	0.304	0.304
Muzzle Velocity	0.000	0.269
Windage	0.000	0.000
Boresight	0.050	0.050
Sabot Discard	0.050	0.050
Aero/Mass Asymmetries	~ 0 . 0 0 0	0.000
Yaw Angle	0.001	0.001
Transverse Velocity	0.058	0.058
Muzzle Spin	0.204	0.204
<i>In-Bore Total (Yaw Rate + Yaw Angle + Transverse Velocity + Muzzle Spin) = 0.371</i>		

4. Comparison Between Experimental and Analytical Results

This project is still a work in progress. The Aerodynamics Branch of ARL and Arrow Tech Associates are continuing the dialog necessary to resolve all the parameters definitions and understand all the translations that may be required to make BALANS output results correlate to the similar quantities that are used in the experimental arena. At the present time, the two parties believe the bottom line quantities of horizontal and vertical standard deviations (sigmas) for total dispersion can be compared directly (see Table 5).

Table 5. Total Dispersion Comparison

Test	Sigma - Horizontal (mrad)	Sigma - Vertical (mrad)
Experiment (10 rounds)	0.470	0.570
Simulation (10 simulations each with 10 rounds)	0.292	0.397
Minimum	0.460	0.533
Maximum	0.369	0.458
Mean (of 10 simulations) Standard Deviation (of 10 simulations)	0.050	0.040

From a strict comparison point of view, the differences between the experimental values and the mean of the simulation values appear to be quite large. However, the difference between the minimum and maximum values of the ten simulations is also significant. This implies that there is some variability in a **10-round** sample size, Another source for the differences is in the number of simulation parameters that had to be estimated.

5. Summary and Conclusions

The full scope of correlating the experimental work with the modeling efforts is incomplete at this time. However, despite the lack of closure on this project, this work has brought the following insights:

- Use of this combined experimental and analytical approach can lead to more effective test plans by providing engineers with the relative magnitude of dispersion improvement to be expected by changes in a configuration.
- The experimental approach complements the analytical approach by providing accurate aerodynamic **coefficients**, a necessary ingredient to determining the free-flight sensitivities for the analytical approach.

- The BALANS analytical approach is useful in the investigation of piece-part dimensional tolerances and their effect on dispersion,
- Since dispersion is a combination of random independent and interdependent events, statistics becomes an important issue. The most important issue is whether one can experimentally predict an overall projectile performance parameter such as dispersion from a lo-round group.
- When combining the experimental approach with the mathematical simulation approach, the modeler should be involved in the experimental methodologies to allow for more understanding of detailed comparisons.

6. References

1. Haug, B. T., and J. A. Bornstein. "Gun Dynamics Measurements for Tank Gun Systems." *Proceedings of the Fifth U.S. Army Symposium on Gun Dynamics*, edited by T. E. Simpkins and C. G. Homan, U.S. Army Armament Research, Development, and Engineering Center, Benet Weapons Laboratories, Watervliet, NY, 1987.
2. Plostins, P., I. Celmins, J. Bornstein, and J. E. Diebler (Battelle Pacific). "The Effects of Sabot Front Borerider Stiffness on the Launch Dynamics of Fin-Stabilized Kinetic Energy Ammunition." **BRL-TR-3047**, U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, MD, October 1989.
3. Arrow Tech Associates. "BALANS Version 2. User's/Technical Manual." South Burlington, VT, August 1998.
4. Arrow Tech Associates. "PRODAS Version 3.9. User's/Technical Manual." South Burlington, VT, January 1998.
5. Hathaway, A. F., and J. R. Burnett, Jr. "Stochastic Approach to Predicting Dispersion." *Proceedings of the 49th Aeroballistic Range Association Meeting*, The Hague, Netherlands, October 1998.

INTENTIONALLY LEFT BLANK.

**NO. OF
COPIES N I Z A T I O N**

**NO. OF
COPIES N I Z A T I O N**

2 DEFENSE TECHNICAL
INFORMATION CENTER
DTIC DDA
8725 JOHN J KINGMAN RD
STE 0944
FT BELVOIR VA 22060-6218

1 DIRECTOR
US ARMY RESEARCH LAB
AMSRL D
RWWHALIN
2800 POWDER MILL RD
ADELPHI MD 20783-I 145

1 HQDA
DAMOFDQ
D SCHMIDT
400 ARMY PENTAGON
WASHINGTON DC 203 1o-0460

1 DIRECTOR
US ARMY RESEARCH LAB
AMSRLDD
J J ROCCHIO
2800 POWDER MILL RD
ADELPHI MD 20783-1145

1 OSD
OUSD(A&T)/ODDDR&E(R)
RJ TREW
THE PENTAGON
WASHINGTON DC 20301-7100

1 DIRECTOR
US ARMY RESEARCH LAB
AMSRL CS AS (RECORDS MGMT)
2800 POWDER MILL RD
ADELPHI MD 20783-1145

1 DPTY CG FOR RDE HQ
us ARMY MATERIEL CMD
AMCRD
MG CALDWELL
5001 EISENHOWER AVE
ALEXANDRIA VA 22333-0001

3 DIRECTOR
US ARMY RESEARCH LAB
AMSRL CI LL
2800 POWDER MILL RD
ADELPHI MD 20783-I 145

1 INST FOR ADVNCD TCHNLGY
THE UNIV OF TEXAS AT AUSTIN
PO BOX 202797
AUSTIN TX 78720-2797

ABERDEEN PROVING GROUND

4 DIR USARL
AMSRL CI LP (305)

1 DARPA
B KASPAR
3701 N FAIRFAX DR
ARLINGTON VA 22203-1714

1 NAVAL SURFACE WARFARE CTR
CODE B07 J PENNELLA
17320 DAHLGREN RD
BLDG 1470 RM 1101
DAHLGREN VA 22448-5100

1 US MILITARY ACADEMY
MATH SCI CTR OF EXCELLENCE
DEPT OF MATHEMATICAL SCI
MAJ M D PHILLIPS
THAYERHALL
WEST POINT NY 10996-1786

**NO. OF
COPIES ORGANIZATION**

**NO. OF
ORGANIZATION**

8 COMMANDER
US ARMY TACOM ARDEC
AMSTA AR CCH B
EFENNEL
R SAYER
B KONRAD
ERIVERA
G EUSTICE
S PATEL
G WAGNECZ
F CHANG
PICATINNY ARSENAL NJ
07806-5000

1 COMMANDER
US ARMY TACOM ARDEC
AMSTA AR FSF T
BLDG 65
C LIVECCHIA
PICATJNNY ARSENAL NJ
07806-5000

3 COMMANDER
US ARMY TACOM ARDEC
AMSTA AR CC
BLDG 65
E GOON
G FLEMING
G MOSHIER
PICATJNNY ARSENAL NJ
07806-5000

5 COMMANDER
US ARMY TACOM ARDEC
AMSTA AR CCH
A MUSALLI
P CHRISTIAN
RCARR
M LUCIANO
TLOUZEIRO
PICATINNY ARSENAL NJ
07806-5000

1 PROGRAM EXECUTIVE OFC
GRND COMBAT & SPRT SYSTMS
SFAE GCSS W BV
S DAVIS
WARREN MI 48397-5000

3 COMMANDER
US ARMY TACOM ARDEC
AMSTA AR FSF DV
K PFLEGER
R TESTA
E LA ROSA
PICATINNY ARSENAL NJ
07806-5000

14 COMMANDER
US ARMY TACOM ARDEC
AMSTA AR FSF T
BLDG 382
S CHUNG
A FARINA
J GRAU
B WONG
W TOLEDO
D PEDERSEN
A FIORELLINI
EVAZQUEZ
CNG
M AMORUSO
W KOENIG
SHAN
GMALEJKO
J THOMASOVICH
PICATINNY ARSENAL NJ
07806-5000

7 ALIANT TECHSYSTEMS INC
R SCHWARTZ
NVLAHAKIS
D FISCHER
R BECKER
S BURRETTA
C AAKHUS
c CANDLAND
600 2ND ST NE
HOPKINS MN 55343

4 ARROW TECH ASSOCIATES INC
RWHYTE
A HATHAWAY
W HATHAWAY
JWHYTE
1233 SHELBURNE RD SUITE D-8
SOUTHBURLINGTON VT 05403

NO. OF
ORGANIZATION

NO. OF
ORGANIZATION

3 PRIMEX TECHNOLOGIES
D **DEMAIRE**
M WILSON
L **WHITMORE**
10101 9TH ST NORTH
ST **PETERSBURG** FL 33702

3 PRTMEXTECHNOLOGIES
B STEWART
J DUCHEK
D OSMENT
PO BOX 127
RED **LION** PA 17356

ABERDEEN PROVING GROUND

1 DIR USATECOM
AMSTETEFLETSIU

1 CDR USA ATC
STEC LI

5 CDR USATACOM ARDEC
AMSTA AR FSF T
R LIESKE
J **MATTS**
F MIRABELLE
RPUHALLA
J **WHITESIDE**

31 DIR USARL
AMSRL WM TD
TFARRAND
K FRANK
AMSRLWM TC
LMAGNESS
AMSRL-WM-TA
M KEELE
AMSRLWMTA
M BURKINS
AMSRLWMT
D **DIETRICH**
AMSRL WM MB
B BURNS
W DRYSDALE
c **HOPPEL**

AMSRL WM B
A HORST
E SCHMIDT
AMSRLWMBA
W D'AMICO
F **BRANDON**
LBTJRKE

AMSRLWMBC
B **GUIDOS**
D LYON
P **PLOSTINS**
JSAHU
P WEINACHT
K SOENCKSEN
D WEBB
J **NEWILL**
S WILKERSON
T ERLINE
CRUTH
J **GARNER**
A **ZIELINSKI**
H EDGE
A **MIKHAIL**
V OSKAY
B PATTON

3 DIR USAMSAA
AMXSY CA
R NORMAN
J CORLEY
R THOMPSON

INTENTIONALLY LEFT BLANK.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
<small>Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.</small>				
1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE January 1999	3. REPORT TYPE AND DATES COVERED Final, Jan 98 - Jan 99		
4. TITLE AND SUBTITLE Dispersion Analysis of the XM881 Armor-Piercing, Fin-Stabilized, Discarding Sabot (APFSDS) Projectile			5. FUNDING NUMBERS 1L162618AH80	
6. AUTHOR(S) Thomas F. Erline and Alan F. Hathaway*				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army Research Laboratory ATTN: AMSRL-WM-BC 4berdeen Proving Ground, MD 21005-5066			8. PERFORMING ORGANIZATION REPORT NUMBER ARL-MR-433	
9. SPONSORING/MONITORING AGENCY NAMES(S) AND ADDRESS(ES)			10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES *Arrow Tech Associates, Inc., 1233 Shelburne Road, Suite D-8, South Burlington, VT 05403				
12a. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution is unlimited.			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) This study compares the results of a dispersion test with mathematical modeling. A 10-round group of modified 25-mm XM881 armor-piercing, fin-stabilized, discarding sabot (APFSDS) projectiles was fired from the M242 chair gun into a designated target. The mathematical modeling results come from BALANS, a product of Arrow Tech Associates. BALANS is a finite-element lumped parameter code that has the capability to model a flexible projectile being fired from a flexible gun. It also has the unique feature of an automated statistical evaluation of dispersion. This study represents an effort to establish a combined experiment and simulation approach to reduce system error.				
14. SUBJECT TERMS dispersion, gun dynamics, projectile dynamics, modeling, experimentation			15. NUMBER OF PAGES 25	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED	20. LIMITATION OF ABSTRACT UL	

INTENTIONALLY LEFT BLANK.

USER EVALUATION SHEET/CHANGE OF ADDRESS

This Laboratory undertakes a continuing effort to improve the quality of the reports it publishes. Your comments/answers to the items/questions below will aid us in our efforts.

1. ARL Report Number/Author ARL-MR-433 (Erline) Date of Report January 1999

2. Date Report Received _____

3. Does this report satisfy a need? (Comment on purpose, related project, or other area of interest for which the report will be used.) _____

4. Specifically, how is the report being used? (**Information** source, design data, procedure, source of ideas, etc.) _____

5. Has the information in this report led to any quantitative savings as far as man-hours or dollars saved, operating costs avoided, or efficiencies achieved, etc? If so, please elaborate. _____

6. General Comments. What do you think should be changed to improve future reports? (Indicate changes to organization, technical content, format, etc.) _____

**CURRENT
ADDRESS**

Organization

Name E-mail Name

Street or P.O. Box No.

City, State, Zip Code

7. **If indicating** a Change of Address or Address Correction, please provide the Current or Correct address above and the Old or Incorrect address below.

**OLD
ADDRESS**

Organization

Name

Street or P.O. Box No.

City, State, Zip Code

(Remove this sheet, fold as indicated, tape closed, and mail.)

(DO NOT STAPLE)